

## CFD Best Practices for Engineering Design

A comprehensive guide to executing accurate, reliable, and actionable CFD simulations—from physics definition through design optimization and engineering decisions.



## 1. Project Framing & PhysicsDefinition

Establishing clear simulation objectives and physics fundamentals ensures CFD delivers actionable engineering insights rather than decorative visualizations.

## Define the Simulation Objective

#### **Critical Question**

State the physical question CFD must answer with quantifiable outputs that directly inform design decisions.

#### **Example Objective**

Estimate pressure drop and velocity uniformity in a 6-tube heat exchanger header operating at 0.2 kg/s mass flow rate.

#### Why This Matters

Without a clear goal, CFD becomes a post-processing exercise that consumes resources without delivering design value. Every simulation must answer: "What decision does this enable?"

- Vague goals like "run CFD to see flow"
- No quantifiable success metrics
- Missing link between results and design decisions

#### Identify Flow Regime & Physics

#### Reynolds Number

Calculate Re to determine laminar, transitional, or turbulent regime—this drives all downstream modeling choices.

#### Time Dependency

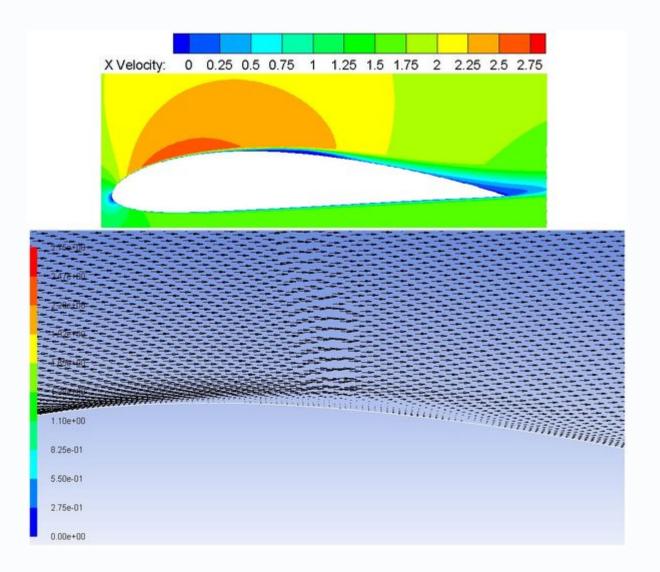
Identify whether flow is steady-state or requires transient analysis for vortex shedding or periodic behavior.

#### Compressibility

Assess Mach number to determine if density variations must be resolved explicitly in the governing equations.

#### Multiphase Nature

Determine if multiple fluid phases, free surfaces, or dispersed particles require specialized modeling approaches.



## Establish Key Outputs & Success Criteria

#### Define Measurable Metrics

- Identify specific engineering parameters to extract :
   pressure drop, heat transfer coefficient, drag coefficient,
   mixing index, or flow uniformity.
- These quantities must be monitored during solution convergence and validated against design requirements or experimental benchmarks.

#### Set Acceptance Thresholds

 Establish numerical targets that define simulation success and guide iterative refinement of geometry or operating conditions. <1 kPa

Target Pressure Drop

Maximum allowable at 0.2 kg/s flow rate

±5%

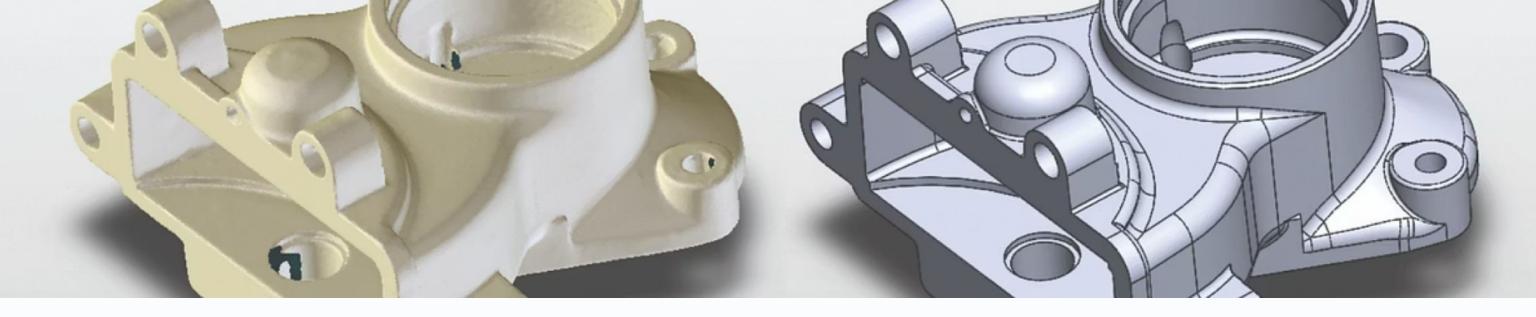
**Velocity Uniformity** 

Across outlet plane cross-section

10-4

Convergence Criteria

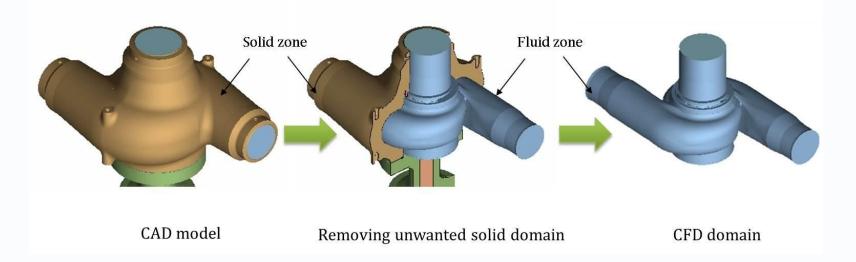
Residual threshold with stable monitors



## 2. Geometry Preparation & Domain Definition

Proper geometry preparation is foundational—a watertight, simplified fluid domain prevents convergence failures and ensures physically meaningful results.

## CAD Cleanup



01

#### **Remove Gaps & Overlaps**

Eliminate surface discontinuities smaller than 0.05 mm that prevent volume extraction. Use Boolean operations to create seamless interfaces.

02

#### **Delete Non-Fluid Components**

Remove bolts, mounting brackets, and structural elements that occupy space but don't affect flow physics.

03

#### **Verify Watertight Volume**

Confirm closed surfaces with consistent normal vectors pointing into the fluid domain—critical for successful meshing.

**Common mistake:** Importing unsealed CAD solids leads to negative volumes and mesh generation failures that consume hours of troubleshooting.

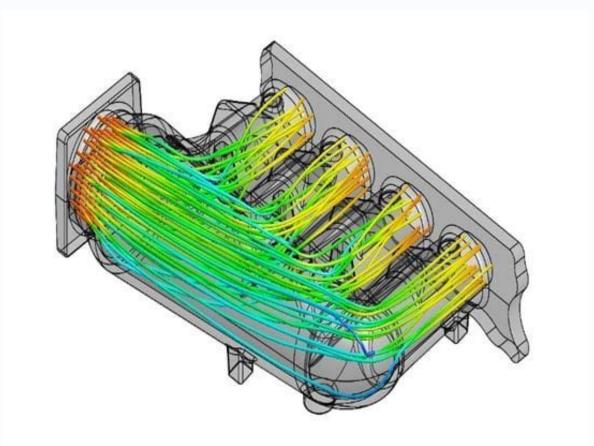
#### Flow Domain Extraction

#### **Subtract Solid Boundaries**

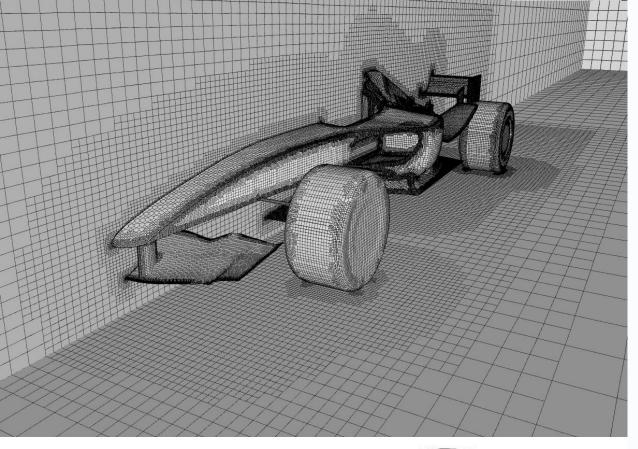
Create the fluid region by performing Boolean subtraction—subtract pipe walls, housing components, and all solid parts from a bounding volume that encompasses the flow path.

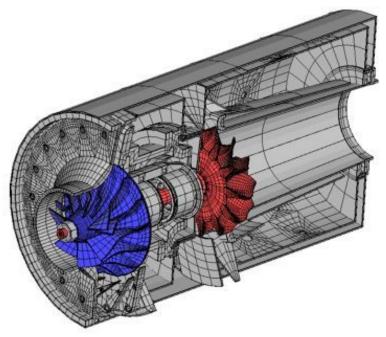
#### Validate Domain Integrity

- Check for open ends that cause non-physical leaks
- Verify inlet and outlet faces are properly defined
- Ensure no isolated fluid pockets remain



**Example:** For an internal manifold, subtract all walls and baffles to obtain the continuous fluid volume where flow equations will be solved.





## 3. Mesh Generation & Quality Control

Mesh quality directly determines solution accuracy—poor meshing causes numerical diffusion, false convergence, and unreliable predictions regardless of physics model sophistication.

## Mesh Type Selection

#### Structured/Hexahedral

Ideal for simple geometries. Provides superior accuracy with fewer cells but requires significant setup effort for complex shapes.

#### **Unstructured/Tetrahedral**

Automatic generation for complex geometry. Requires more cells for equivalent accuracy—avoid for boundary-layer-dominated flows without prism layers.

#### **Polyhedral**

Balances automation with accuracy.

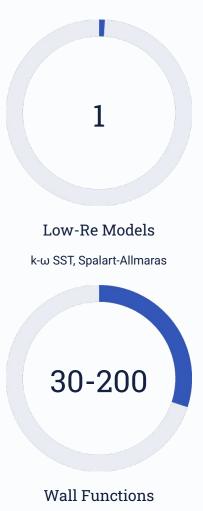
Reduces cell count by 30-50% versus
tetrahedral while maintaining solution
quality for industrial applications.

**Recommended approach:** Hexahedral core with prismatic inflation layers at walls combines efficiency with accurate boundary layer resolution.

#### **Boundary Layer Meshing**

#### Y+ Control Strategy

The dimensionless wall distance Y+ determines whether viscous sublayer is resolved or modeled via wall functions—critical for accurate wall shear stress and heat transfer.



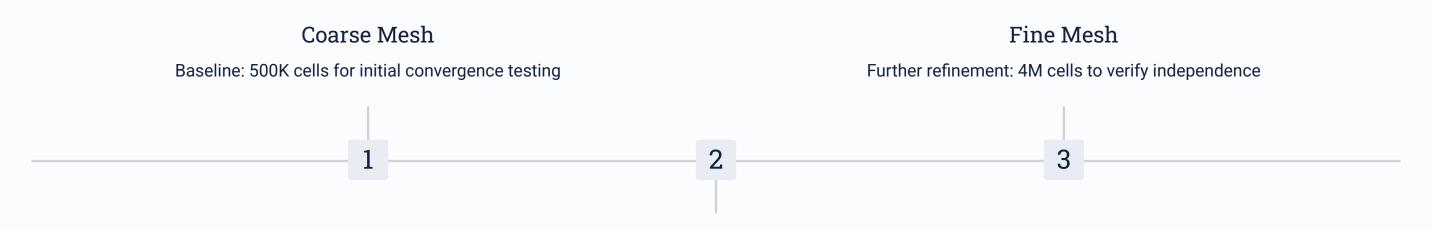
Standard k-ε models

#### **Prism Layer Requirements**

- L. Minimum 5 layers for gradient resolution
- Growth ratio  $\leq 1.2$  for smooth transitions
- 3. First cell height computed from target Y+
- . Consistent resolution across all walls

Common mistake: Single inflation layer or Y+ mismatch with turbulence model yields incorrect friction factors and heat transfer coefficients.

#### Mesh Independence Study



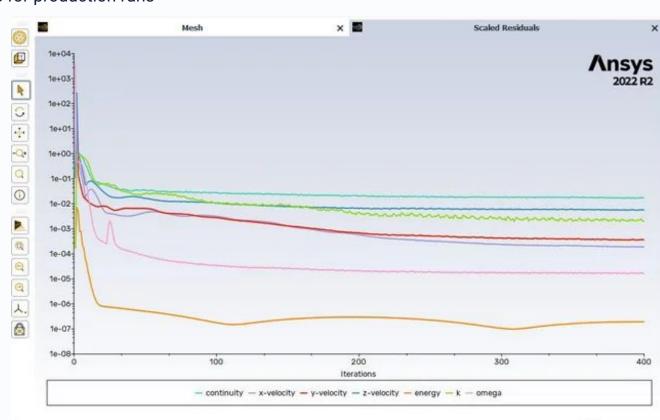
2× refinement: 1.5M cells for production runs

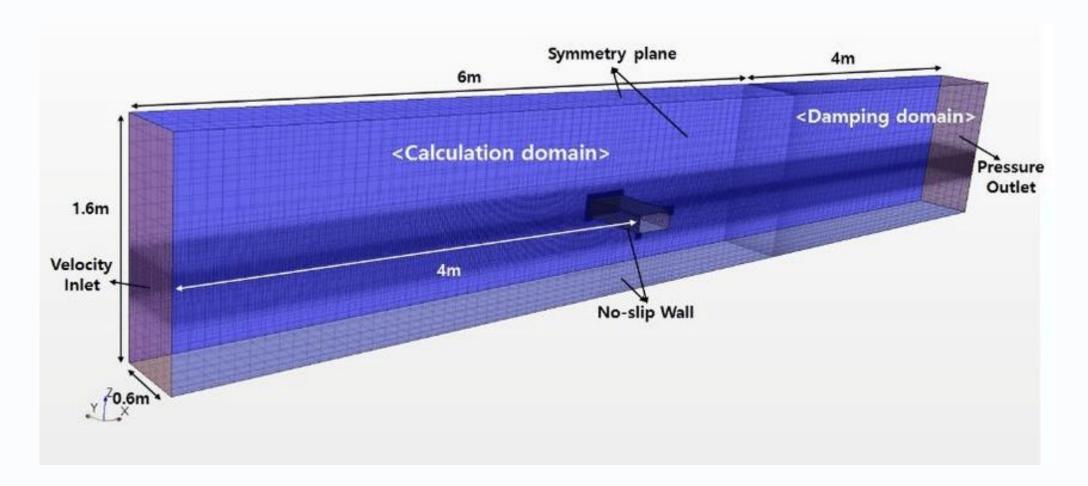
Medium Mesh

#### Convergence Criteria

Solution is mesh-independent when key engineering parameters change by less than 2% between successive refinements. Monitor:

- Global quantities (ΔP, drag, heat flux).
- Local values at critical locations.
- Profile distributions across planes.





## 4. Boundary Conditions & Physical Models

Accurate boundary conditions and physics selection determine whether CFD captures real-world behavior—wrong choices invalidate even the finest mesh.

#### Define Inlets & Outlets



#### Mass Flow Inlet

Specify mass flow rate when total flow is known—solver distributes flow based on resistance. Include turbulence intensity (typically 1-10%) and hydraulic diameter.



#### Velocity Inlet

Use when flow distribution is prescribed.

Requires velocity magnitude and direction—suitable for uniform developed profiles or CFD-mapped distributions.



#### **Pressure Outlet**

Static pressure boundary (gauge or absolute). Allows backflow if solution requires—use target mass flow rate to stabilize initial iterations.

**Critical Rule:** Never over-specify—setting both inlet velocity AND outlet flow rate creates mathematical inconsistency. Pressure-based solvers require one velocity/mass-flow boundary and one pressure boundary.

#### Wall & Symmetry Conditions

#### Wall Boundary Properties

No-slip condition: Zero velocity at wall (standard for viscous flows)
Roughness height: Equivalent sand-grain roughness in microns
Thermal condition: Adiabatic, constant temperature, or heat flux

Motion: Stationary, rotating, or translating reference frame

#### **Symmetry Plane Guidelines**

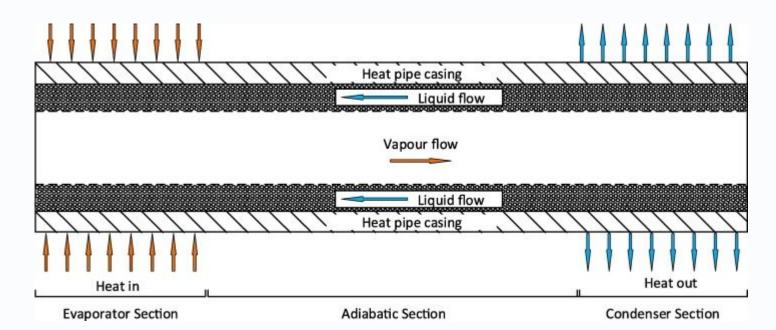
Use only when geometry AND flow field are truly symmetric. Zero normal gradients enforced—inappropriate for asymmetric separation or vortices.

**Example Configuration** 

**Pipe walls:** Adiabatic, smooth (Ks = 0)

**Heated surface:** 350 K constant temperature

Symmetry: Midplane for symmetric manifold



## Physical Model Setup



#### Turbulence Modeling

k-ω SST: Best for adverse pressure gradients, separation.
k-ε Realizable: Good for free shear flows. LES/DES: For transient vortex-dominated flows with sufficient resolution.



#### **Energy Equation**

Enable when temperature variations affect density, viscosity, or are outputs of interest. Include viscous dissipation for high-speed flows.



#### **Radiation Models**

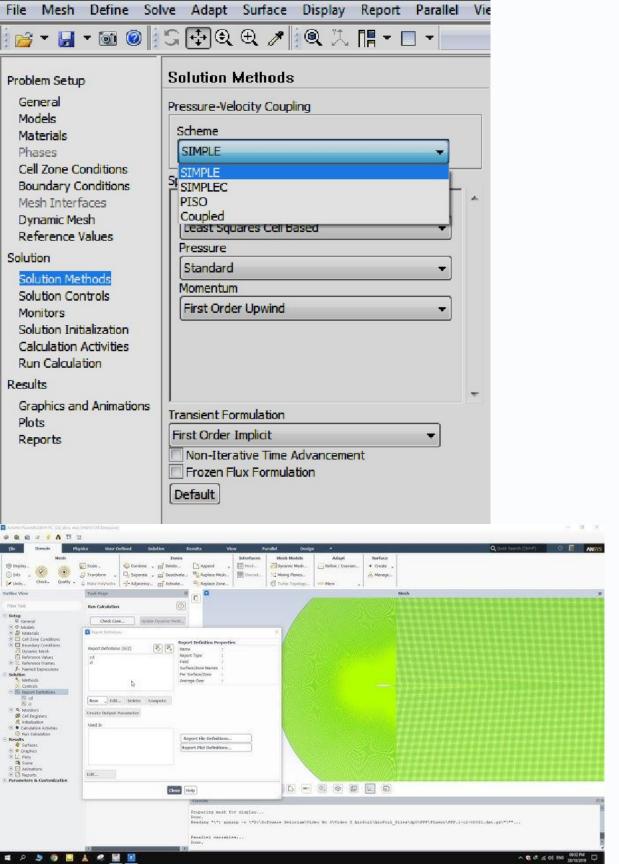
Discrete Ordinates (DO) or Surface-to-Surface (S2S) for combustion, furnaces, or high-temperature systems where radiation heat transfer is significant.



#### Multiphase Models

VOF for free surfaces, Eulerian for dispersed bubbly flows, DPM for dilute particle tracking—choose based on volume fraction and coupling strength.

**Engineering judgment:** Activate only necessary models—unnecessary physics increases computational cost and introduces instability without improving accuracy for your specific engineering question.



## 5. Solver Setup & Numerical Controls

Solver configuration and discretization schemes control numerical stability and accuracy—even correct physics fails with poor numerics.

#### Solver Type & Formulation

#### Pressure-Based Solver

Default for incompressible and low-speed compressible flows (Mach < 0.3). SIMPLE or SIMPLEC algorithm couples pressure and velocity through continuity constraint. Robust for most industrial applications.

#### **Density-Based Solver**

Required for high-speed compressible flows (Mach > 0.3) where density variations are significant. Solves coupled momentum and continuity simultaneously—better for supersonic nozzles, turbomachinery.

#### Steady vs. Transient

Use steady-state for time-independent flows to save computational cost. Switch to transient when capturing vortex shedding, pulsatile flow, or periodic phenomena—requires appropriate time step selection.

**Example:** Compressible nozzle flow (Mach 1.8)  $\rightarrow$  density-based coupled solver with transient formulation, time step  $\Delta t = 1 \times 10^{-6}$  s based on acoustic CFL condition.

#### **Discretization Schemes**

#### **Spatial Discretization**

First-order upwind: Stable but diffusive—use only for initial iterations

Second-order upwind: Production standard—balances accuracy and stability

QUICK/MUSCL: Third-order accuracy for refined meshes and smooth flows

#### **Temporal Discretization**

First-order implicit: Unconditionally stable, acceptable for slow transients

Second-order implicit: Preferred for accurate transient phenomena

Under-relaxation factors control solution stability—reduce from defaults (0.7 momentum, 0.3 pressure) for difficult cases.

2nd

Momentum

Second-order upwind scheme

2nd

Time Integration

Second-order implicit

0.7

#### **Relaxation Factor**

Momentum equation

Common mistake: Using first-order everywhere produces smeared gradients and incorrect separation locations—visual results look reasonable but quantitative outputs are wrong.

### Residuals 100 $10^{-1}$ 10<sup>-2</sup> omega Residuals [ - ] 10<sup>-3</sup> 10<sup>-5</sup> $10^{-6}$ 10-7 10-8 80000 Iterations [ - ]

### Convergence & Residuals

01

#### Set Residual Targets

Continuity, momentum: 10<sup>-4</sup> for most flows. Energy: 10<sup>-6</sup> for accurate heat transfer. Stricter for precision applications.

02

#### **Monitor Key Quantities**

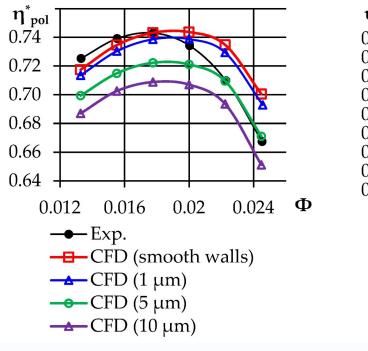
Track integral values: mass flow rate, forces, pressure drop, average temperatures. Solution is converged when these stabilize, not just residuals.

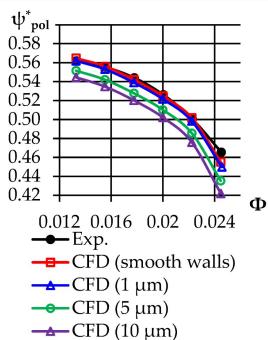
03

#### **Verify Stationarity**

Check that monitored quantities oscillate with <1% amplitude for at least 200 iterations after residuals plateau—true indication of convergence.

**Critical insight:** Residual drop indicates equation balance, but physical convergence requires stable engineering outputs. A  $10^{-3}$  residual with oscillating drag coefficient means the solution has not converged.





## 6. Verification & Validation

Verification confirms correct equation solution; validation confirms correct physics representation—both are essential for engineering confidence in CFD predictions.

### Mass & Energy Balance Check

#### Conservation

#### Verification

Fundamental laws must be satisfied within numerical tolerance. Post-process to confirm:

- Mass flow rate: inlet = outlet (±0.1%)
- Energy: total enthalpy flux conserved
- Momentum: forces balance pressure and shear

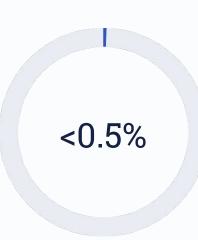
#### Imbalance

#### Diagnosis

Persistent imbalance > 1% indicates:

- Non-converged solution
- Poor mesh quality near boundaries
- Incorrect boundary condition specification





**Energy Imbalance** 

Acceptable for thermal cases

Common mistake: Accepting 2% mass imbalance as "close enough"—this compounds through the domain and invalidates quantitative predictions.

## Grid Convergence Index (GCI)

1

2

3

#### Richardson Extrapolation

Estimate exact solution by
extrapolating grid-refined sequence to
zero cell size

#### Calculate GCI

Quantify discretization uncertainty as percentage of solution value

#### **Report Confidence**

State engineering result with numerical uncertainty bounds

GCI methodology (Roache 1998) requires three meshes with constant refinement ratio  $r \approx 1.3-2.0$ . Calculate apparent order of accuracy and discretization error estimate.

**Example:** Pressure drop predictions: Coarse mesh = 985 Pa, Medium = 964 Pa, Fine = 959 Pa  $\rightarrow$  GCI = 2.5%  $\rightarrow$  Report:  $\Delta$ P = 959 ± 24 Pa with 95% confidence.

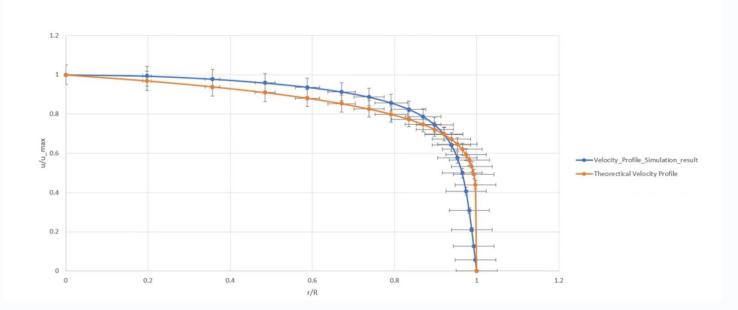
#### Validation with Analytical / Empirical Data

#### **Comparison Strategy**

- 1. Identify relevant benchmark: analytical solution, correlation, or experimental data
- 2. Match all conditions: geometry, Re, boundary conditions, measurement locations
- 3. Compare appropriate quantities: friction factor, Nusselt number, drag coefficient
- 4. Document deviations and assess acceptability

**Acceptance criteria:** Agreement within  $\pm 5\%$  for well-established flows;  $\pm 10$ -15% for complex geometries with experimental uncertainty.





#### **Example Validation**

Turbulent pipe flow at Re = 50,000

**CFD:** f = 0.0182

**Moody chart:** f = 0.0177

Deviation: +2.8% ✓

Common mistakes: Comparing static pressure to total pressure; neglecting entrance length effects in pipe flow validation; using inappropriate Reynolds number definition.

# 7. Post-Processing & Interpretation

Effective visualization and quantitative extraction transform numerical results into engineering insights—thoughtful post-processing reveals the physics story.

#### Visualization & Streamlines

#### Flow Patterns

Streamlines reveal pathlines, separation zones, and recirculation regions that govern pressure loss and mixing performance.

#### Scalar Fields

Contour plots display pressure,
temperature, velocity magnitude on
planes or surfaces—use consistent scales
for comparison.

#### **Vector Displays**

Arrows indicate local direction and magnitude—essential for understanding complex 3D flow structures and vorticity.

**Best practices:** Use sufficient seed points for streamlines (50-100), select representative plane locations, annotate key features, and maintain consistent color scales across design iterations for meaningful comparison.

### **Quantitative Data Extraction**

#### Objective

Derive  $\Delta P$ , forces, heat flux, etc.

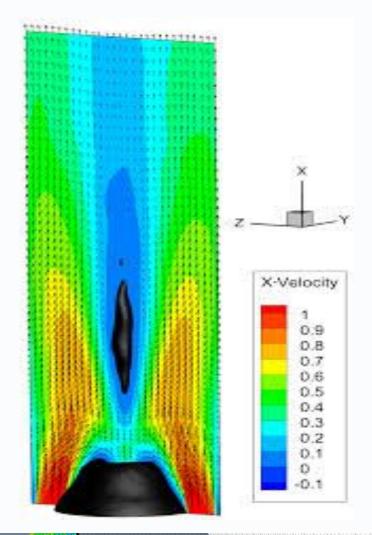
#### Why important

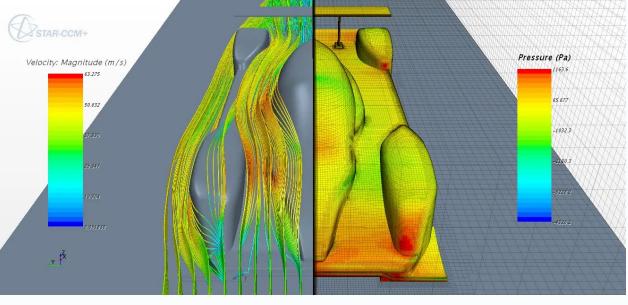
Design decisions depend on these metrics.

#### Example

Average Nusselt number = 85;  $\Delta P = 0.9$  kPa.

- Extracting from single cell instead of area-average
- Inconsistent reference pressure or units





## Turbulence & Boundary Layer Review

#### Objective

Inspect Y+, turbulence kinetic energy, wall shear stress.

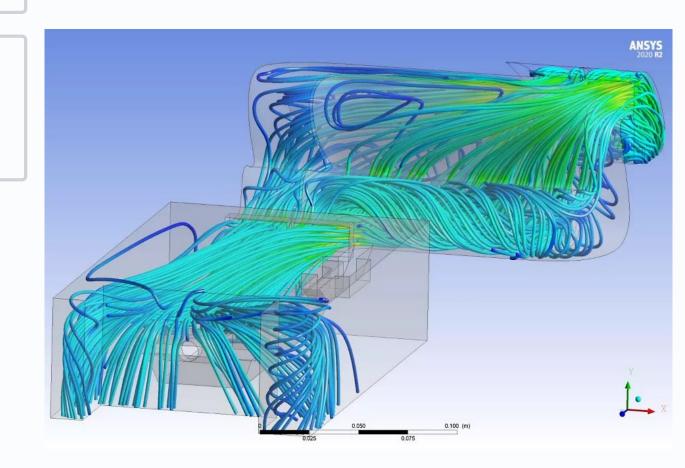
#### Why important

Detects poor near-wall resolution.

#### Example

Y+ < 1 across 95% wall area.

- Ignoring regions with Y+ > 300
- Averaging Y+ over entire wall indiscriminately



### Thermal Analysis Results

#### Objective

Review temperature fields, heat transfer coefficients.

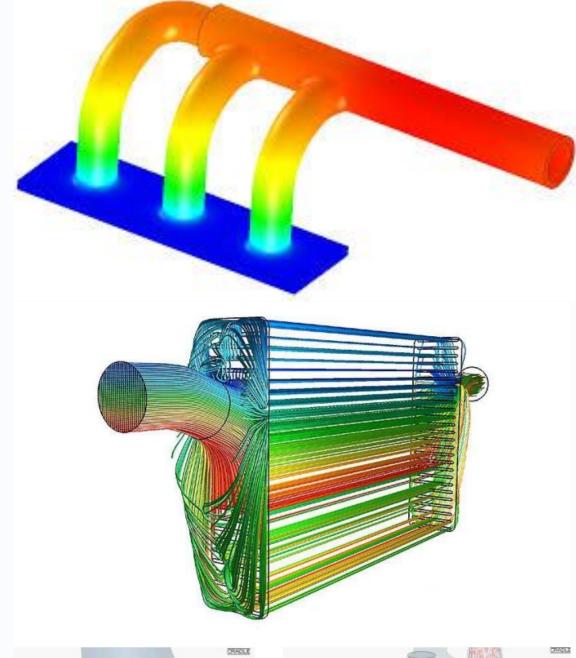
#### Why important

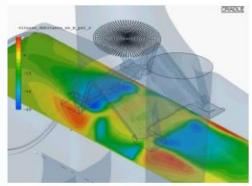
Ensures realistic gradients and heat flux continuity.

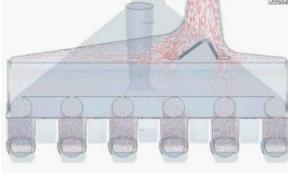
#### Example

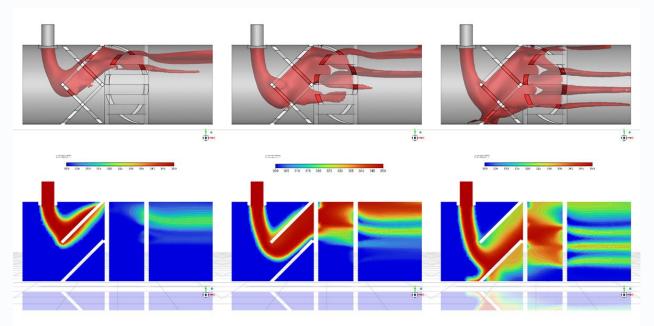
Hot spot at outlet = 105 °C vs. target < 90 °C.

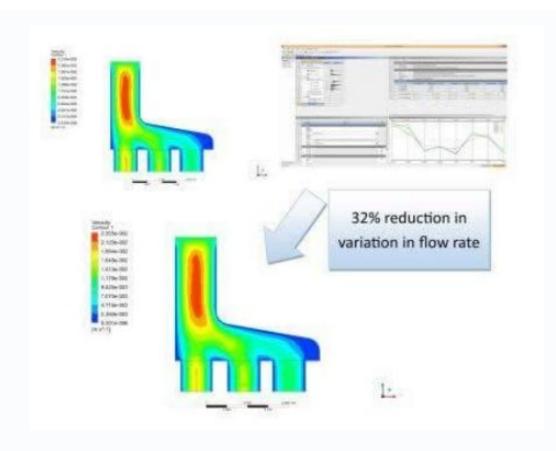
- Non-converged thermal fields
- Using default emissivity = 1.0 in radiation











## 8. Design Optimization & Sensitivity

Design optimization and sensitivity analysis transform CFD from analysis tool to design enabler—systematic parameter studies reveal optimal configurations and quantify design robustness.

#### Parametric Studies

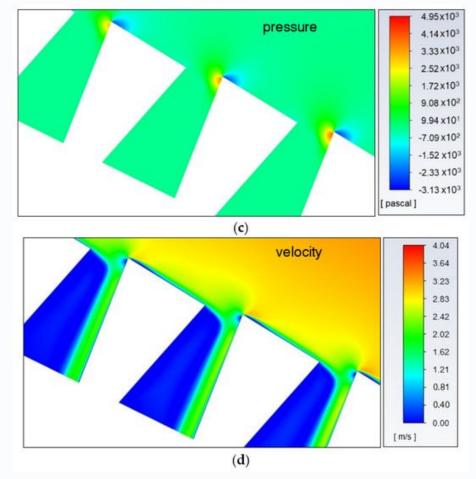
#### Objective

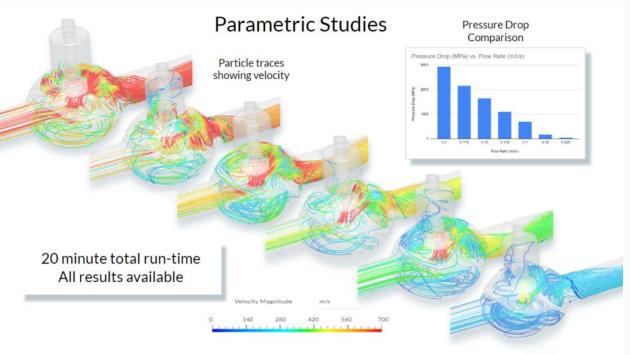
Evaluate performance vs. geometry/operating changes.

#### Why important

Identifies design levers.

- Changing multiple parameters without DOE planning
- Comparing unconverged runs





### Sensitivity & Uncertainty Quantification

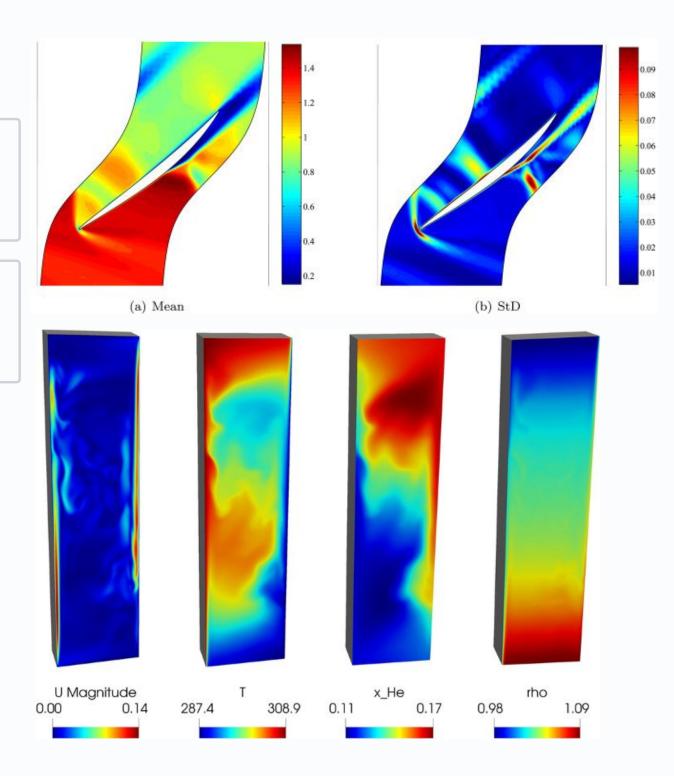
#### Objective

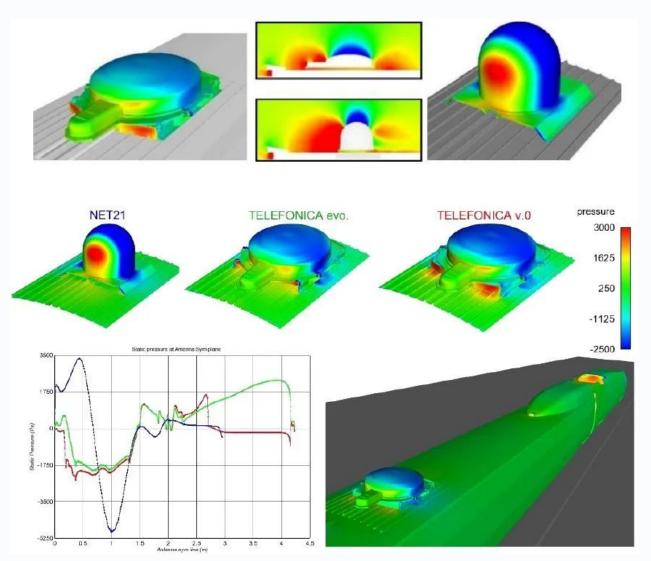
Assess variability impact on results.

#### Why important

Shows design robustness.

- Ignoring turbulence intensity variations
- Assuming deterministic results for stochastic inputs





## 9. Reporting & Engineering Decision

Proper reporting transforms CFD results into actionable engineering decisions and institutional knowledge—comprehensive documentation ensures repeatability while clear insights drive design improvements.

## **Documentation & Traceability**

#### Objective

Record all setup parameters, models, and key results.

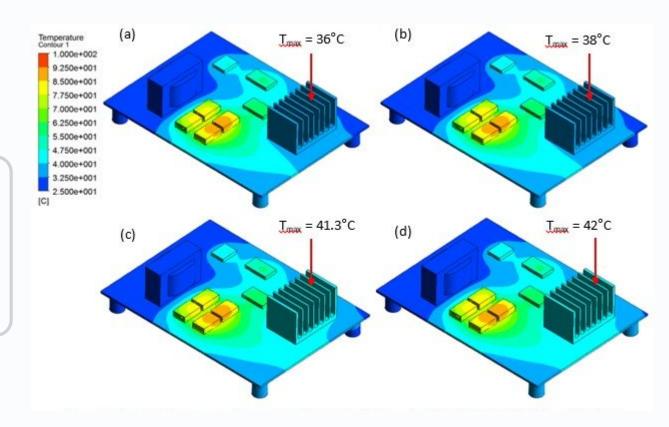
#### Why important

Enables repeatability and peer review.

#### Example

Include domain image, mesh stats, residual plots, boundary summary.

- Missing solver version, model, or mesh count
- Inconsistent naming or units



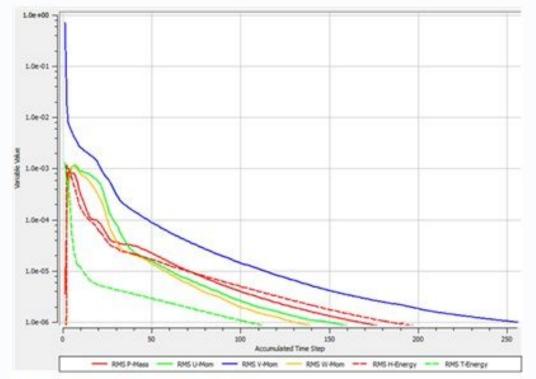


Figure 1 - Example Residual Monitors

## Engineering Insights & Design Actions

#### Objective

Translate results into tangible recommendations.

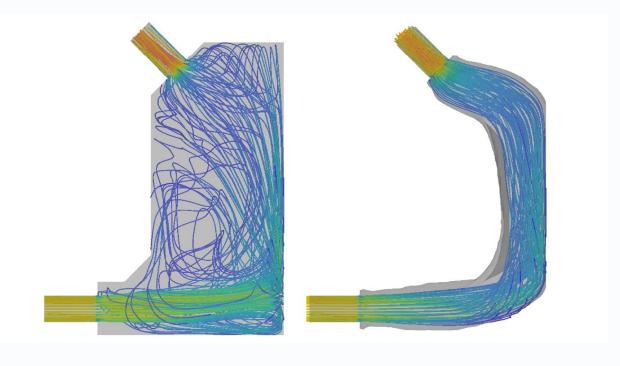
#### Why important

CFD's value = design improvement.

#### Example

Add guide vane  $\rightarrow$  velocity uniformity +12%,  $\Delta P$  +1.5%.

- Reporting beautiful images without design action
- Over-interpreting marginal results (< 3% change)</li>



## Lessons Learned & Future Simulations

#### Objective

Capture learnings for next iteration.

#### Why important

Builds institutional knowledge.

#### Example

Next run: include radiation + finer wall mesh.

#### Common mistakes:

Not updating simulation best-practice checklist